

Analysis of Spent Ion Exchange Media: Superlig 639 and Superlig 644

D. E. Kurath
J. J. Wagner

May 2000

Prepared for BNFL, Inc. under
Project 29953

LEGAL NOTICE

This report was prepared by Battelle Memorial Institute (Battelle) as an account of sponsored research activities. Neither Client nor Battelle nor any person acting on behalf of either:

MAKES ANY WARRANTY OR REPRESENTATION, EXPRESS OR IMPLIED, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, process, or composition disclosed in this report may not infringe privately owned rights; or

Assumes any liabilities with respect to the use of, or for damages resulting from the use of, any information, apparatus, process, or composition disclosed in this report.

References herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by Battelle. The views and opinions of authors expressed herein do not necessarily state or reflect those of Battelle.

Analysis of Spent Ion Exchange Media: Superlig 639 and Superlig 644

D. E. Kurath
J. J. Wagner

May 2000

Battelle, Pacific Northwest Division
Richland, Washington 99352

Summary

The current BNFL Inc. flowsheet for the pretreatment of the Hanford high-level tank wastes includes the use of Superlig[®] materials^(a) for removing ¹³⁷Cs and ⁹⁹Tc from the aqueous fraction of the waste. The cesium-selective Superlig[®] 644 (SL-644) and the technetium-selective Superlig[®] 639 (SL 639) materials have been evaluated in tests with actual waste samples. These materials have a finite processing lifetime in the plant and will need to be disposed of. The composition and level of residual radionuclide contamination is important for assessing various disposal pathways for the spent Superlig[®] materials.

This report contains the results of analyzing subsamples of the SL-639 and SL 644 materials that have been used in small-column testing of actual waste samples at the Radiochemical Processing Laboratory. The wastes that have been tested include samples from Tanks 241-AW-101 (Envelope A) and 241-AN-107 (Envelope C). The spent resins were analyzed with inductively coupled plasma/atomic emission spectrometry (ICP-AES) for metals, cold vapor atomic absorption (CVAA) spectroscopy for mercury, gamma energy analysis (GEA) for radionuclides, and inductively coupled plasma/mass spectrometry (ICP-MS) for selected metals and radionuclides.

The analytes of interest that were detected at levels above the minimum reportable quantities (MRQs) are given in Table S1. The results for both samples contain the contribution from interstitial liquid, which was <0.1 M NaOH for SL-644 and deionized (DI) water for SL-639. All specified MRQs were readily met, and the quality control checks met the requirements of the governing quality assurance (QA) plan. Since the detection limits were generally well below the MRQs, the concentrations of many other analytes of interest may be found in the body of the report. While these results provide an indication of the analyte concentrations that may be left on the spent resin, they do not fully represent the concentrations that may be found after extended plant processing with additional load/elute cycles and different waste compositions.

(a) These materials have been developed and supplied by IBC Advanced Technologies, Inc., American Fork, Utah.

Table S1. Analytes of Interest Detected at Levels Above the MRQs

Analyte	SL-644	SL-639	MRQ	Method
	µg/g	µg/g	µg/g	
Cr	670	--	100	ICP-AES
K	220	160	60	
Na	83,800	--	5,400	
⁹⁹ Tc	6.74	6.95	2.0	ICP-MS
²³⁸ U	14.8	--	6.0	
	µCi/g	µCi/g	µCi/g	
⁶⁰ Co	1.31	--	0.12	GEA
¹³⁷ Cs	21.3	--	0.01	

Terms and Abbreviations

BNFL	BNFL, Inc; subsidiary of British Nuclear Fuels, Ltd.
BV	bed volume
C/C_0	analyte concentration in column effluent divided by analyte concentration in feed
CVAA	cold vapor atomic absorption
DI	deionized water
GEA	gamma energy analysis
ICP-AES	inductively coupled plasma/atomic emission spectrometry
ICP-MS	inductively coupled plasma/mass spectrometry
MDL	method detection limit
MRQ	minimum reportable quantity
QA	quality assurance
RPP-WTP	River Protection Project-Waste Treatment Plant

Contents

Summary	iii
Terms and Abbreviations	v
1.0 Introduction	1.1
2.0 Experimental	2.1
2.1 SL-644 Processing History.....	2.1
2.2 SL-644 Sample Preparation and Analyses	2.2
2.3 SL-639 Processing History.....	2.2
2.4 SL-639 Sample Preparation and Analyses	2.3
3.0 Results And Discussion	3.1
3.1 ICP-AES Results	3.1
3.2 CVAA Results for Mercury	3.4
3.3 Results of Gamma Energy Analysis	3.4
3.4 Results of ICP-MS Analyses.....	3.6
4.0 Conclusions	4.1
5.0 References	5.1

Figures

Figure A.1. Flow sheet for Analytical Preparation of SL-644	A.1
Figure A.2. Flow sheet for Analytical Preparation of SL-639	A.2

Tables

Table S1. Analytes of Interest Detected at Levels Above the MRQs.....	iv
Table 2.1. Final ^{137}Cs and C/C_0 Values for the SL-644 Columns Used in Actual Waste Testing.....	2.1
Table 2.2. Final ^{95}Tc C/C_0 values for the SL-639 Columns Used in Actual Waste Testing	2.3
Table 3.1. ICP-AES Analysis of Spent SL-644 and SL-639 Resins and the MRQs	3.2
Table 3.2. Comparison of ICP-AES Results for Spent SL-644 and SL-639 Resins to Cesium Ion Exchange Feed Concentrations	3.3
Table 3.3. CVAA Mercury Analysis of Spent Resin and the MRQ	3.4
Table 3.4. GEA Results for the Spent Resin and MRQs.....	3.5
Table 3.5. Interstitial Liquid Radiochemical Results by Gamma Energy Analysis.....	3.5
Table 3.6. ICP-MS Analysis of Spent SL-644 Resin and the Minimum Reportable Quantities	3.6

1.0 Introduction

The current BNFL Inc. flowsheet for the pretreatment of the Hanford High-Level tank wastes includes the use of Superlig[®] materials^(a) for the removal of ¹³⁷Cs and ⁹⁹Tc from the aqueous fraction of the waste. The cesium-selective Superlig[®] 644 (SL-644) and the technetium-selective Superlig[®] 639 (SL-639) have been evaluated in tests with actual waste samples. These materials have a finite processing lifetime in the plant and will need to be disposed of. The composition and level of residual radionuclide contamination is important for assessing various disposal pathways for the Superlig[®] materials.

This report contains the results of analyses of subsamples of the SL-639 and SL 644 materials that have been used in small column testing of actual waste samples at the Radiochemical Processing Laboratory. The wastes that have been tested include samples from Tanks 241-AW-101 and 241-AN-107 (the 241 prefix is common to all Hanford tanks and will not be used hereafter). The analyses of the spent resins include inductively coupled plasma/atomic emission spectrometry (ICP-AES) for metals, cold vapor atomic absorption (CVAA) spectroscopy for mercury, gamma energy analysis (GEA) for radionuclides and inductively coupled plasma/mass spectrometry (ICP-MS) for selected metals and radionuclides.

While these results provide an indication of the analyte concentrations that may be left on the spent resin, they do not fully represent the concentrations that may be found after extended plant processing with additional load/elute cycles and different waste compositions. BNFL estimates that the SL-644 may last for 100 load/elute cycles with Envelope A and C wastes and 20 cycles with Envelope B wastes.^(b) The number of useable load/elute cycles for the SL-639 is not well defined, but is likely on the order of hundreds.

(a) These materials have been developed and supplied by IBC Advanced Technologies, Inc., American Fork, Utah.

(b) Specification 7 of Contract No. DE-RP06-96RL13308.

2.0 Experimental

This section describes the sample processing history for the SL-644 and SL-639 resins and discusses the resin subsampling and preparation for the analytical procedures.^a

2.1 SL-644 Processing History

The SL-644 resin was used in a small dual-column ion exchange system to remove cesium from samples of Tanks AW-101 (Envelope A) and AN-107 (Envelope C). The AW-101 sample was processed in June 1999 with the conduct of two complete loading cycles. Both columns were loaded, rinsed with deionized (DI) water, eluted with 0.5 M nitric acid, rinsed with DI water, and regenerated with 0.1 M NaOH (Kurath et al. 1999). The second loading cycle was conducted with the same AW-101 sample to remove residual cesium that was not removed during the first cycle. The AN-107 sample was processed in October 1999 with a single load/elute cycle. All process steps were similar to those used in processing the AW-101 sample (Kurath et al. 2000). Since both columns were eluted after each run, the order of the columns was not switched.

The extent to which ¹³⁷Cs was removed from the columns before analysis is indicated in Table 2.1. The ¹³⁷Cs concentration and the ¹³⁷Cs C/C₀ values (analyte concentration in column effluent divided by analyte concentration in feed) are shown for the final eluate samples for both columns and for the final rinse sample and composite regeneration sample for Column 1. The C₀ value is 153 μCi/mL and corresponds to the ¹³⁷Cs concentration found in the AN-107 cesium ion exchange feed sample. For reference, the target end point for elution is a C/C₀ = 1E-02.

Table 2.1. Final ¹³⁷Cs and C/C₀ Values for the SL-644 Columns Used in Actual Waste Testing

	Column 1		Column 2	
	¹³⁷ Cs Concentration μCi/mL	¹³⁷ Cs C/C ₀	¹³⁷ Cs Concentration μCi/mL	¹³⁷ Cs C/C ₀
Final Eluate Sample	9.1E-01	5.9E-03	0.73	4.8E-03
Final Rinse Sample	5.5E-02	3.6E-04	ND	ND
Composite Regeneration sample	2.3E-02	1.5E-04	ND	ND

ND = Not determined.

The total amount of SL-644 initially added to the columns was 8.6 g (4.3 g/column) on a dry basis (at 95°C) in the hydrogen form. When the resin was removed from the columns, it was in the sodium form in contact with dilute caustic (<0.1 M NaOH). The total volume of the resin beds just before removal from the columns was 40.7 mL. This volume is expanded relative to the 30 mL of resin observed during the

^a Information related to sample preparation may be found in the laboratory record book BNW 13687, pages 19-22. Analytical results were obtained under Analytical Service Request # 5732.

loading step in the processing of the AW-101 sample and the 34.5 mL observed during the loading step in the processing of the AN-107 sample.

2.2 SL-644 Sample Preparation and Analyses

The resin from both columns was removed into separate jars for removal from the hot cells. DI water from a squirt bottle was used to wash all of the resin from the columns. Excess liquid above the settled resin was removed with a syringe, but the resin remained submerged in liquid. Since some dilution of the interstitial liquid occurred, the concentration of NaOH was less than the 0.1 M used to regenerate the columns in the last process step. Once the jars had been transferred to a fume hood, the contents were combined and manually mixed. The liquid in contact with the resin was a very dark, nearly opaque brown color.

Separate 10-mL subsamples of the wet resin (10.0262 g) and the liquid were obtained in 20-mL scintillation vials and counted directly for the GEA. The resin subsample was then dried at 95°C until a steady mass of 1.1532 g was obtained. The preparative method used to dissolve the resin was selected based on previous work with resin materials. The resin was dissolved on a best-effort basis, and no attempt was made to validate the preparative method for the analytes of interest. However, the method is considered to be applicable to the resin matrix and the analytes measured. In summary, the dried subsample was dissolved in hot nitric acid (16 M) with the aid of hydrogen peroxide (50%), taken to near-dryness, and then diluted with water to a final volume of 20 mL with a nitric acid concentration of about 0.3 M. A flow diagram of the resin-preparation steps may be found in Appendix A. Separate 10-mL aliquots of the dissolved resin were used for ICP-AES following procedure PNNL-ALO-211 and ICP-MS following procedure PNNL-ALO-280. During the preparation of the wet resin subsample, excess liquid was removed from above the resin with a pipette, but the settled resin was kept in a fully submerged state. Consequently, the analytical results for the resin contain the contribution from the interstitial liquid.

Another portion of the SL-644 wet resin was air dried to a constant mass. Subsamples (≈ 0.1 g) of the air-dried resin were processed and diluted to a volume of 25 mL following digestion procedure PNNL-ALO-131. The mercury level was determined using CVAA spectroscopy following procedure PNNL-ALO-201. Separate subsamples of the air-dried resin were further dried in an oven at 95°C to determine the f-factor (ratio of oven-dried mass to air-dried mass). This information was used to adjust the mercury concentrations to a dry basis (at 95°C).

2.3 SL-639 Processing History

The SL-639 was used in a small dual-column ion exchange system to remove Tc from samples of Tanks AW-101 and AN-107. Both samples had been previously processed for cesium removal with SL-644. The AW-101 sample was processed first in July 1999 (Blanchard et al. 1999), and this was followed about 16 weeks later in early November by processing the AN-107 sample (Blanchard et al. 2000). Following the processing of the AW-101 sample, the lead column was eluted with 0.5 M nitric acid. The positions of the lead and lag columns were switched so that the partially loaded lag column

became the lead column for the next sample. Following the processing of the AN-107 sample, the lead column was eluted with water at $\approx 50^{\circ}\text{C}$. Some additional experimentation was completed in which some AN-107 simulant was passed through the column and then some additional actual AN-107 sample. At the completion of these experiments, both columns were partially loaded so additional elution was conducted. Approximately 225 mL (48 bed volumes [BVs]) of DI water at 50°C was used to elute the first column. The initial 19 BVs were pumped through the column at a flow rate of 3 BV/h, and the remaining 29 BVs were pumped at a rate of 1.5 BV/h. The second column was eluted with 0.5 M nitric acid at ambient temperature since switching the heating system to the second column would have been difficult. The volume of nitric acid used was about 363 mL (77 BVs). The flow rate was maintained at 3 BV/h. Several BVs of DI water were used to flush nitric acid from the system.

The extent to which Tc was removed from the columns before analysis is indicated in Table 2.2. The $^{95}\text{Tc } C/C_0$ value is shown for the final aliquot from each elution. The ^{95}Tc was added to the samples in trace amounts as ammonium pertechnetate (NH_4TcO_4) in 1 M NaOH to follow the progress of the testing. The samples along with the original AN-107 Tc IX sample were counted in a portable GEA instrument. The C_0 value corresponds to the ^{95}Tc level found in the feed sample and was determined as counts per 3-min count time. For both columns, the desired elution cutoff of $C/C_0 = 1\text{E-}02$ was not obtained. This cutoff was also not obtained during the actual sample testing due to a very slow decline in Tc concentration that resulted in large volumes of eluate.

Table 2.2. Final $^{95}\text{Tc } C/C_0$ Values for the SL-639 Columns Used in Actual Waste Testing

	Column 1	Column 2
	$^{95}\text{Tc } C/C_0$	$^{95}\text{Tc } C/C_0$
Final Eluate Sample	0.053	0.036

The total amount of SL-639 added to both columns was 9.4 mL or 4.5 g on a dry basis (at 95°C). Unlike the SL-644, this material does not exhibit an appreciable change in volume when in contact with the various processing solutions. Consequently, the resin BV just before removal from the columns was unchanged.

2.4 SL-639 Sample Preparation and Analyses

The resin plus interstitial DI water from both columns was removed with a plastic bulb pipette and combined in a single container. After mixing, separate subsamples of the wet resin (2.9321 g, 2.55 mL) and the liquid (1.9288 g, 2 mL) were added to 20-mL scintillation vials and counted directly for the GEA following procedure PNNL-ALO-450. The resin subsample was then dried at 95°C until a steady resin mass of 1.2251 g was obtained. The preparative method used to dissolve the resin by dry ashing and acid dissolution of the residue was selected based on previous work with resin materials. The resin was dissolved a best-effort basis, and no attempt was made to validate the preparative method for the analytes of interest. However, the method is considered to be applicable to the resin matrix and the analytes measured. In summary, the dried resin was ashed at 450°C , and the ash was dissolved in 16 M nitric acid

on a hotplate, reduced in volume to ≈ 0.5 mL, and then diluted with water to 20 mL with a nitric acid concentration of about 0.3 M. A flow diagram of the resin preparation steps may be found in Appendix A. Aliquots of this solution were used for ICP-AES following procedure PNNL-ALO-211 and ICP-MS following procedure PNNL-ALO-280. During the preparation of the wet resin subsample, excess liquid was removed from above the resin with a pipette, but the settled resin was kept in a fully submerged state. Consequently, the analytical results for the resin contain the contribution from the interstitial liquid.

Another portion of the SL-639 was air dried to a constant mass on filter paper. Subsamples (≈ 0.1 g) of the air-dried resin were processed and diluted to a volume of 25 mL per procedure PNNL-ALO-131. The mercury level was determined using CVAA spectroscopy following procedure PNNL-ALO-201. Separate subsamples of the air-dried resin were further dried in an oven at 95°C to determine the f-factor (ratio of oven dried mass to air dried mass). This information was used to adjust the mercury concentrations to a dry basis (at 95°C).

3.0 Results And Discussion

This section contains the results of the analyses conducted on the SL-644 and SL-639 spent resin samples. The results of the analyses include ICP-AES (metals), CVAA (mercury), GEA (radionuclides) and ICP-MS (selected metals and radionuclides). The analytical reports and calculations may be found in Appendix B.

3.1 ICP-AES Results

The results of the analysis of the SL-644 and SL-639 spent resin samples with ICP-AES are shown in Table 3.1 along with the BNFL specified minimum reportable quantities (MRQs). Analytes of interest (i.e., those with specified MRQs) are given in the upper portion of the table while other analytes that were detected are given in the lower portion. All concentrations are based on the mass of the resin samples dried at 95°C. The results for both samples contain the contribution from the interstitial liquid: <0.1 M NaOH for SL-644 and DI water for SL-639. The analytes of interest that were detected in the SL-644 sample at levels above the MRQs include Cr, K and Na. Potassium was the only analyte of interest detected in the SL-639 sample at levels above the MRQs. All specified MRQs were readily met and the quality control checks met the requirements of the governing quality assurance (QA) plan.

The results from Table 3.1 are given on a volume basis (10 mL for SL-644 and 2.55 mL for SL-639) in Table 3.2 and compared to the compositions of the cesium ion exchange (Cs IX) feeds. The compositions of the cesium ion exchange feeds were obtained from Kurath et al (1999) and Kurath et al (2000). The components that appear to have concentrated on the SL-644 resin relative to the feed concentrations include Cr, Co, and Zr. Other metals that are found on the SL-644 resin in significant amounts include Ca, Cu, Fe, Na, Ni, Pb, Sr, and Zn. For SL-639, the only component that appears to be slightly concentrated relative to the feed is Fe. Other metals found on the SL-639 resin in significant amounts include Cr, Mn, Na, and Sr. The presence of these components indicates that the resins likely have some affinity for these metals.^a Processing of additional waste quantities or types, as will occur in the River Protection Project-Waste Treatment Plant (RPP-WTP), could result in higher levels of these metals in the resins. The high concentration of Na in the SL-644 resin is due to the resin being mainly in the sodium form and from the interstitial liquid. For both resin samples, a significant portion of the boron and silicon present is likely from leaching of the glassware used in the sample preparation.

^a Results not contained in this report indicate that the SL-639 and SL-644 resins do not contain appreciable quantities of these components.

Table 3.1. ICP-AES Analysis of Spent SL-644 and SL-639 Resins and the MRQs

Analytes of Interest	SL-644	SL-639	MRQ
	µg/g	µg/g	µg/g
Ag	5.04	<0.24	100
Al	60.9	[6.5]	3,600
Ba	[0.58]	[0.41]	600
Ca	147	[9.9]	6,000
Cd	[0.56]	<0.24	20
Cr	669	5.0	100
Cu	116	[1.1]	600
Fe	84.2	30.4	1,200
K	[220]	[160]	60
La	<0.43	<0.4	3,000
Mg	[5.7]	[6.2]	5,400
Mn	0.92	1.63	300
Na	83,800	2,300	5,400
Ni	51.5	[4.4]	1,800
Pb	10.9	<1	30
Ti	4.02	[0.15]	600
Zn	20.6	[0.45]	1,200
Other Analytes Measured			
As	<1.4	[1.9]	--
B	170	88.9	--
Bi	[9.8]	<1.6	--
Co	70.9	<0.4	--
P	[9.1]	[6.4]	--
Pd	<5.2	[6.9]	
Ru	[1.4]	<1.2	--
Si	22.8	39.7	--
Sr	1.57	2.4	--
Th	[14]	<13	--
Zr	181	<0.4	--

Notes:

1. Overall error for results greater than 10-times the method detection limit (MDL) is estimated to be +/- 15%.
2. Results in brackets [] are within 10 times the MDL with errors likely to exceed 15%.
3. Less than (<) indicates the result is less than the MDL.
4. The dashes (--) indicate that no MRQ was specified.
5. The dissolution preparations (both wet ashing and dry ashing) were performed on a best-effort basis; i.e., dissolution procedures were not validated.

Table 3.2. Comparison of ICP-AES Results for Spent SL-644 and SL-639 Resins to Cesium Ion Exchange Feed Concentrations

Analytes of Interest	SL-644	SL-639	AW-101 Cs IX Feed	AN-107 Cs IX Feed
	µg/mL	µg/mL	µg/mL	µg/mL
Ag	0.58	<0.09	<0.6	<1
Al	7.0	[3.1]	11,100	2,450
Ba	[0.07]	[0.20]	<0.4	<0.4
Ca	17	[4.8]	5.6	170
Cd	[0.06]	<0.09	1.5	29
Cr	77	2.4	43	46
Cu	13	[0.5]	4.9	20
Fe	9.7	14.6	14	[11]
K	[25]	[77]	15,600	[780]
La	<0.05	<0.16	<1	<2
Mg	[0.7]	[3.0]	<4	<4
Mn	0.106	0.78	1.6	2.9
Na	9,660	1,100	105,500	119,200
Ni	5.9	[2.1]	4.4	240
Pb	1.3	<0.4	27	67
Ti	0.46	[0.07]	<0.2	<1
Zn	2.4	[0.22]	5.2	[6.7]
Other Analytes Measured				
As	<0.16	[0.9]	18	<10
B	20	43.2	73	36
Bi	[1.1]	<0.8	<4	<4
Co	8.2	<0.2	<1	2.5
P	[1.0]	[3.1]	222	310
Pd	<0.6	[3.3]	<12	<30
Ru	[0.2]	<0.6	<3	<45
Si	2.6	19.1	221	[49]
Sr	0.18	1.16	<0.2	136
Th	[2]	<6.3	<32	<40
Zr	21	<0.2	2.1	2.5

Notes:

1. Overall error for results greater than 10-times the MDL is estimated to be +/- 15%.
2. Results in brackets [] are within 10 times the MDL with errors likely to exceed 15%.
3. Less than (<) indicates the result is less than the MDL.
4. The dissolution preparations (both wet ashing and dry ashing) were performed on a best-effort basis; i.e., dissolution procedures were not validated.

3.2 CVAA Results for Mercury

The results of the analysis of the SL-644 and SL-639 spent-resin samples with CVAA for mercury are shown in Table 3.3 along with the BNFL-specified MRQ. The results are given on a mass basis and are based on the mass of the ≈ 0.1 g resin samples. The mass basis of the resin samples is adjusted to a dry basis at 95°C using f-factors (ratio of oven-dried mass to air-dried mass). The f-factor was 0.824 for SL-644 and 0.988 for SL-639. The results for both samples contain a minimal contribution from the interstitial liquid since most of the liquid was absorbed by the filter paper on which the samples were air dried. The MRQ was readily met for all samples. The level of mercury found in all of the resin samples is comparable to the levels found in the process blanks, so it appears that there is no appreciable quantity of mercury present in the resin samples.

In general, the quality control checks met the requirements of the governing QA plan with the exception of the matrix spike. The recovery of the matrix spike (27%) was below the acceptance criteria of 75% to 125%. The high-carbon content in the resin may have caused failure of the matrix spike by requiring more oxidizing reagent than was available. Recovery of the post spike was 105%, well within the acceptance criteria of 75% to 125%. Since the post-spike recovery was acceptable, it also implies that low recovery of the matrix spike was related to sample digestion.

Table 3.3. CVAA Mercury Analysis of Spent Resin and the MRQ

Sample	Concentration	MRQ
--	$\mu\text{g/g}$	$\mu\text{g/g}$
SL-644	0.23	1.5
SL-639	0.13	1.5
process blank-1	0.19	--
process blank-2	0.12	--

3.3 Results of Gamma Energy Analysis

The results of the GEA of the SL-644 and SL-639 spent resin samples are shown in Table 3.4 along with the BNFL specified MRQs. The results given on a mass basis ($\mu\text{g/g}$) in the second and third columns are based on the mass of the resin samples dried at 95°C. The results given on a volume basis in columns 5 and 6 are based on the resin sample volumes; 10 mL for SL-644 and 2.55 mL for SL-639. The results for both samples contain the contribution from the interstitial liquid, which was <0.1 M NaOH for SL-644 and DI water for SL-639. All specified MRQs were readily met, and the quality control checks met the requirements of the governing QA plan. The presence of ^{95}Tc and $^{95\text{m}}\text{Tc}$ is the result of adding a ^{95}Tc tracer to the waste samples to monitor the Tc ion exchange experiment. The analytes of interest that were detected in the SL-644 sample at levels above the MRQs include ^{60}Co and ^{137}Cs . No analytes of interest were found in the SL-639 sample at concentrations above the MRQs.

Table 3.4. GEA Results for the Spent Resin and MRQs

	SL-644	SL-639	MRQ	SL-644	SL-639
	μCi/g	μCi/g	μCi/g	μCi/mL	μCi/mL
⁶⁰ Co	1.31E+00	3.45E-04	1.2E-01	1.51E-01	1.66E-04
¹³⁷ Cs	2.13E+01	7.5E-05	1.0E-02	2.46E+00	3.6E-05
¹⁵⁴ Eu	6.59E-03	1.93E-03	3.0E-01	7.6E-04	9.25E-04
¹⁵⁵ Eu	1.43E-02	1.83E-03	6.0E+00	1.65E-03	8.78E-04
¹²⁵ Sb	<2.6E-02	<3.3E-04	--	<3E-03	<1.6E-04
¹³⁴ Cs	1.64E-02	<7.4E-05	--	1.89E-03	<3.5E-05
¹⁴⁴ CePr	<3.5E-02	<8.0E-04	--	<4E-3	<4E-04
²⁴¹ Am	8.93E-03	1.07E-03	--	1.03E-03	5.13E-04
⁹⁵ Tc	--	2.64E-02	--	--	1.27E-02
^{95m} Tc	--	5.58E-01	--	--	2.68E-01

Note: -- indicates that no value was specified.

The results of the GEA of the interstitial liquid samples are shown in Table 3.5 along with the ratio of the concentrations (given as %) in the liquid to the ratio of the concentrations in the resin plus liquid sample. These results are based on the liquid-sample volumes of 10 mL for the dilute caustic (<0.1 M NaOH) in contact with the SL-644 resin and 2 mL for the DI water in contact with the SL-639. The relatively low-percentage values indicate that most of the radioactivity detected in the resin plus liquid samples was associated with the resin.

Table 3.5. Interstitial Liquid Radiochemical Results by Gamma Energy Analysis

	SL-644	SL-644 liquid:resin	SL-639	SL-639 liquid:resin
	μCi/mL	%	μCi/mL	%
⁶⁰ Co	8.2E-03	5.4	<6E-06	0
¹³⁷ Cs	1.6E-02	0.65	<7E-06	0
¹⁵⁴ Eu	1.4E-04	17.9	6.3E-05	8.5
¹⁵⁵ Eu	9.3E-05	5.7	3.7E-05	5.3
¹²⁵ Sb	5.0E-05	ND	<2E-05	ND
¹³⁴ Cs	2.3E-04	12.2	<6E-06	ND
¹⁴⁴ Ce ¹⁴⁴ Pr	6.1E-05	ND	<4E-05	ND
²⁴¹ Am	2.4E-04	22.8	3.4E-05	8.4
⁹⁵ Tc	--	ND	2.1E-05	0.21
^{95m} Tc	--	ND	3.5E-04	0.16

Notes: -- indicates that no value was provided. ND = not determined because one or both values for ratio were at the MDL.

3.4 Results of ICP-MS Analyses

The results of analyzing the SL-644 and SL-639 spent-resin samples with ICP-MS are shown in Table 3.6 along with the BNFL-specified MRQs. The results given on a mass basis ($\mu\text{g/g}$) in the second and third columns are based on the mass of the resin samples dried at 95°C . The results given on a volume basis are based on the original volume of the resin samples; 10 mL for SL-644 and 2.55 mL for SL-639. The results contain the contribution from the interstitial liquid; <0.1 M NaOH for SL-644 and DI water for SL-639. The analytes of interest that were detected in the SL-644 sample at levels above the MRQs include ^{99}Tc and ^{238}U . For the SL-639 sample, only ^{99}Tc was detected at levels above the MRQs. All specified MRQs were readily met, and the quality control checks met the requirements of the governing QA plan.

Table 3.6. ICP-MS Analysis of Spent SL-644 Resin and the Minimum Reportable Quantities

	SL-644	SL-639	MRQ	SL-644	SL-639
	$\mu\text{g/g}$	$\mu\text{g/g}$	$\mu\text{g/g}$	$\mu\text{g/mL}$	$\mu\text{g/mL}$
As	2.86E-01	2.13E+00	2.3E+00	3.3E-02	1.02E+00
Se	$<6.3\text{E-}02$	6.7E-02	2.0E+01	$<7.3\text{E-}03$	3.2E-02
Tl	1.87E-01	$<5.4\text{E-}03$	6.0E+00	2.2E-02	$<2.6\text{E-}03$
V	9.3E-02	1.36E-02	6.0E+00	1.1E-02	6.5E-03
^{99}Tc	6.74E+00	6.95E+00	2.0E+00	7.8E-01	3.34E+00
$^{126}\text{Sn}^{(1)}$	1.2E-02	$<2.2\text{E-}03$	6.0E+00	1.4E-03	$<1\text{E-}03$
^{127}I	2.0E-02	$<8.6\text{E-}03$	3.0E+01	2.0E-03	$<4.1\text{E-}03$
^{129}I	$<4.7\text{E-}03$	3.3E-03	--	$<5\text{E-}04$	1.6E-03
^{233}U	$<5.2\text{E-}03$	$<2\text{E-}03$	6.0E-01	$<6\text{E-}04$	$<1\text{E-}03$
^{234}U	$<2.6\text{E-}03$	$<1\text{E-}03$	6.0E+00	$<3\text{E-}04$	$<5\text{E-}04$
^{235}U	1.52E-01	$<2\text{E-}03$	6.0E+00	1.8E-02	$<1\text{E-}03$
^{236}U	1.5E-02	$<2\text{E-}03$	6.0E+00	1.7E-03	$<1\text{E-}03$
^{238}U	1.48E+01	2.1E-02	6.0E+00	1.71E+00	1.0E-02
^{237}Np	4.7E-02	$<2.2\text{E-}03$	6.0E+00	5.4E-03	$<1.1\text{E-}03$
^{239}Pu	6.6E-02	$<2\text{E-}03$	6.0E+00	7.7E-03	$<1\text{E-}03$
$^{240}\text{Pu}^{(1)}$	1.4E-02	$<2\text{E-}03$	6.0E+00	1.6E-03	$<1\text{E-}03$
$^{241}\text{AMU}^{(2)}$	$<5.2\text{E-}03$	$<2\text{E-}03$	TBD by method	$<6\text{E-}04$	$<1\text{E-}03$
$^{242}\text{AMU}^{(2)}$	$<5.2\text{E-}03$	$<2\text{E-}03$	TBD by method	$<6\text{E-}04$	$<1\text{E-}03$
$^{243}\text{AMU}^{(2)}$	$<5.2\text{E-}03$	$<2\text{E-}03$	TBD by method	$<6\text{E-}04$	$<1\text{E-}03$

(1) Calculated from response of different isotope. Results should be considered semiquantitative.

(2) AMU-242 calculated using Pu-242. AMU-241,243 calculated using Am-241, Am-243.

4.0 Conclusions

The following conclusions can be drawn from these studies.

- The analytes of interest that were above the MRQs for the SL-644 resin include Cr, K, Na, ^{60}Co , ^{99}Tc , ^{137}Cs , and ^{238}U .
- The analytes of interest that were above the MRQs for the SL-639 resin include K and ^{99}Tc .
- Based on the ICP-AES results, the components that appear to have concentrated (relative to the waste samples processed) on the SL-644 include Cr, Co, and Zr. For the SL-639 resin, the only component that appears to be slightly concentrated is Fe. The presence of these components indicates that the resins likely have some affinity for these metals.
- No significant level of mercury was found in either of the Superlig samples.
- The analytical methods met the MRQs for all analytes of interest.

5.0 References

Blanchard, DL, Jr, DE Kurath, and JR Bontha. 1999. *Small Column Testing of Superlig 639 for Removal of ^{99}Tc from Hanford Tank Waste Envelope A (Tank 241-AW-101)*, BNFL-RPT-016 (draft), PNWD-3004, Battelle Pacific Northwest Division, Richland, Washington.

Blanchard, DL, Jr, DE Kurath, and BM Rapko. 2000. *Small Column Testing of Superlig 639 for Removal of ^{99}Tc from Hanford Tank Waste Envelope C (Tank 241-AN-107)*, BNFL-RPT-022 (draft), PNWD-3028, Battelle Pacific Northwest Division, Richland, Washington.

Kurath, DE, DL Blanchard, Jr, and JR Bontha. 1999. *Small Column Ion Exchange Testing of Superlig 644 for Removal of ^{137}Cs from Hanford Tank Waste Envelope A (Tank 241-AW-10)*, BNFL-RPT-014 (draft), PNWD-3001, Battelle Pacific Northwest Division, Richland, Washington.

Kurath, DE, DL Blanchard, Jr, and JR Bontha. 2000. *Small Column Ion Exchange Testing of Superlig 644 for Removal of ^{137}Cs from Hanford Tank Waste Envelope C (Tank 241-AN-107)*, BNFL-RPT-024 (draft), PNWD-3039, Battelle Pacific Northwest Division, Richland, Washington.

Appendix A

Resin Sample Preparation Flow Diagrams

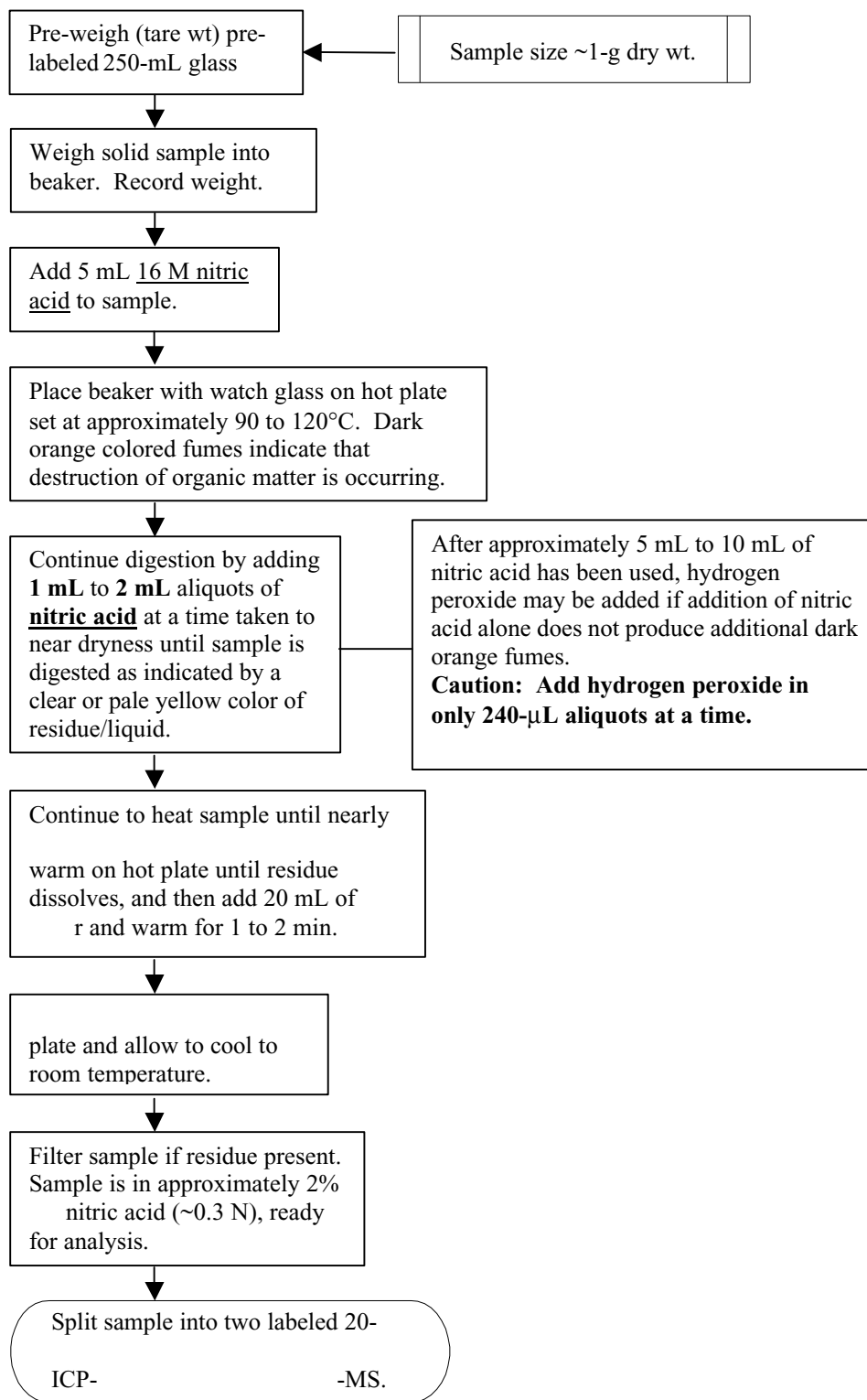


Figure A.1. Flowsheet for Analytical Preparation of SL-644

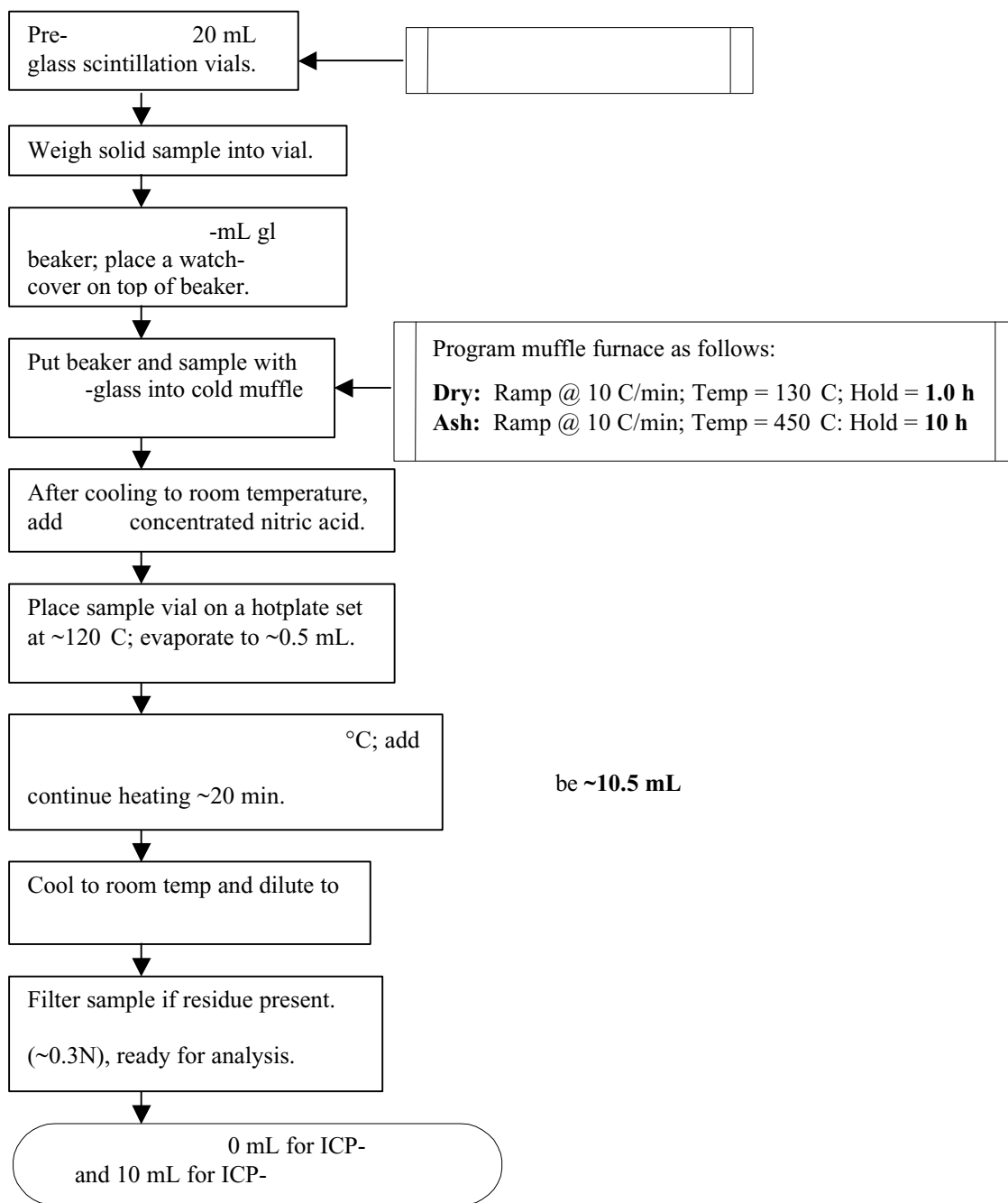


Figure A.2.

-639

Appendix B

Analytical Results and Analysis

Sample Identification

Sample ID	Sample Number	Description
SL 644-	00 1367	-644 resin sample + interstitial liquid
SL- -SR	00-	SL 639 resin sample + interstitial liquid
-644 LQ	-1369	Interstitial liquid in contact with the SL- (<0.1 M NaOH)
SL- -LQ	00-	Interstitial liquid in contact wit -639 resin sample (DI water)

1) Analytical Service Request # 5732

Appendix A

Resin Sample Preparation Flow Diagrams

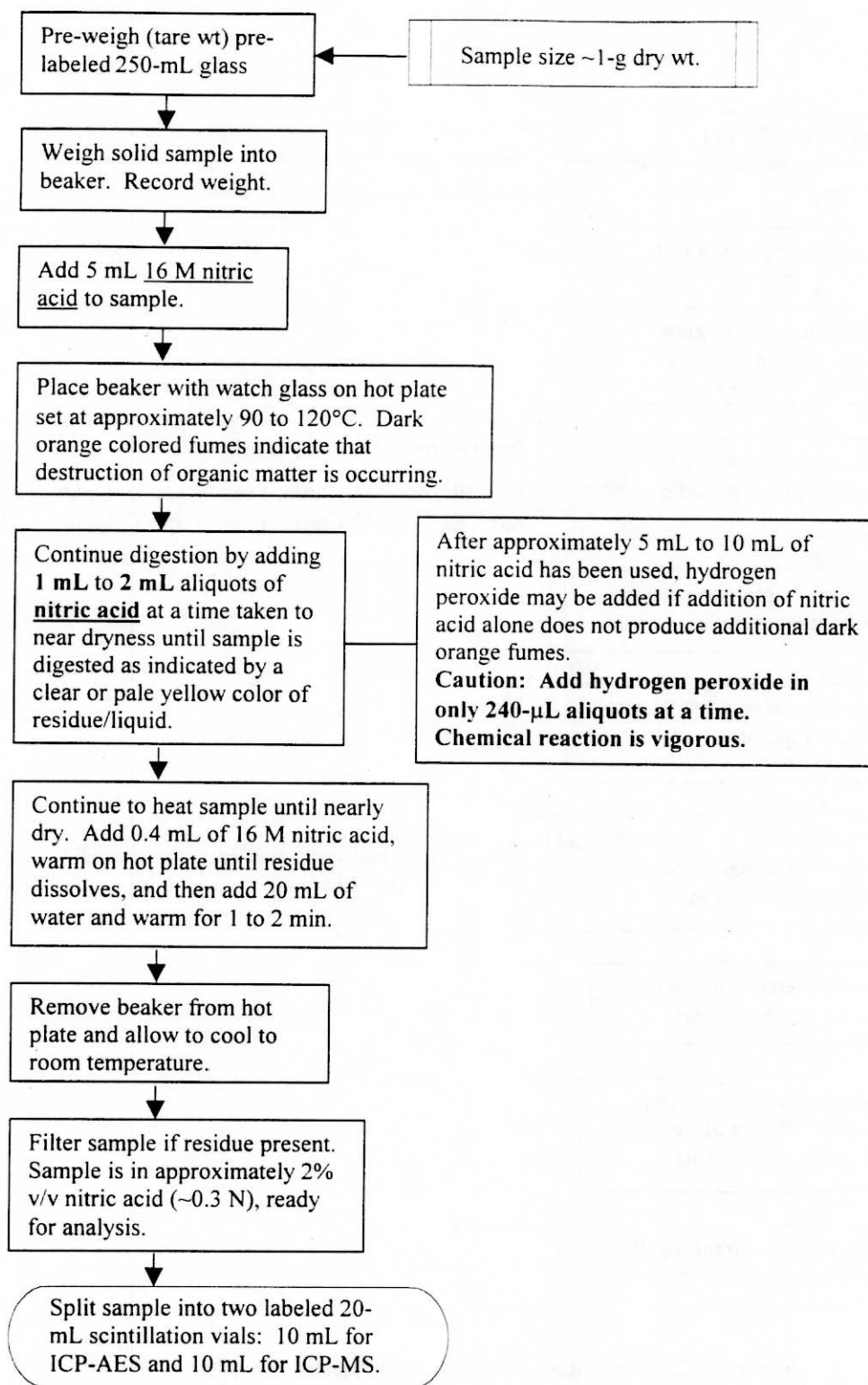


Figure A.1. Flowsheet for Analytical Preparation of SL-644

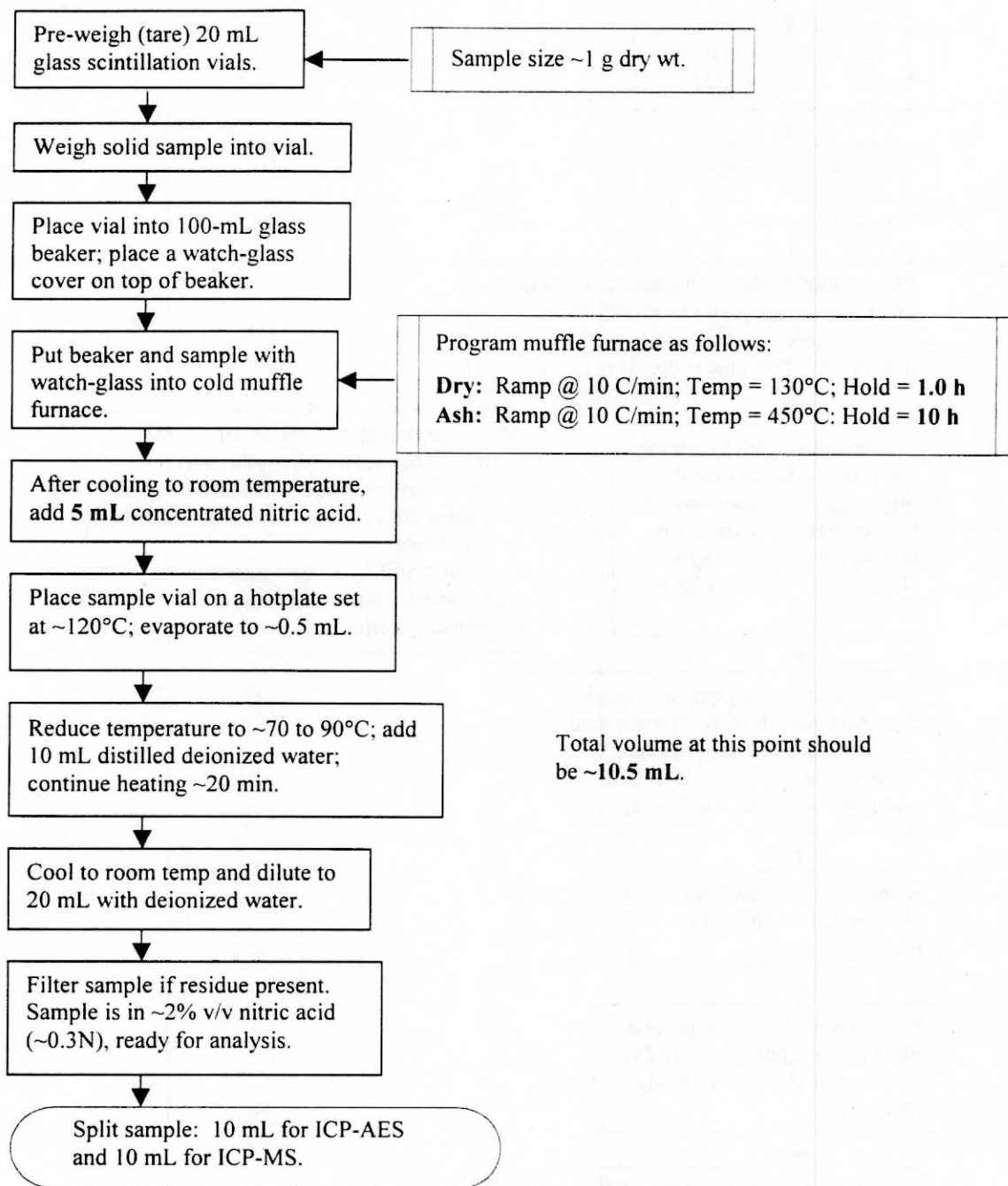


Figure A.2. Flow sheet for Analytical Preparation of SL-639

Appendix B

Analytical Results and Analysis

Sample Identification

Sample ID	Sample Number	Description
SL-644-SR	00-1367	SL-644 resin sample + interstitial liquid
SL-639-SR	00-1368	SL-639 resin sample + interstitial liquid
SL-644-LQ	00-1369	Interstitial liquid in contact with the SL-644 resin sample (<0.1 M NaOH)
SL-639-LQ	00-1370	Interstitial liquid in contact with the SL-639 resin sample (DI water)

Note: 1) Analytical Service Request # 5732

**Battelle PNNL/RPG/Inorganic Analysis ...
ICPAES Data Report**

Project: 29953
Client: D. Kurath

RPL Number(s): 00-01367 & 00-01368

Client ID: "SL-644-SR" through "SL-639-SR"

ASR Number: 5732

Total Samples: 2

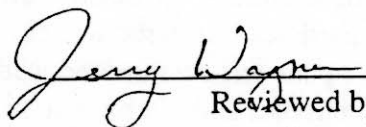
Procedure: PNL-ALO-211, "Determination of Elements by Inductively Coupled
Argon Plasma Atomic Emission Spectrometry" (ICP-AES).

Analyst: D.R. Sanders

Analysis Date (Filename): 03-15-00 (A0589)

See Chemical Measurement Center 98620: ICP-325-405-1 File for Calibration and
Maintenance Records.

M&TE Number: ICPAES instrument -- WB73520
Mettler AT400 Balance -- Ser.No. 360-06-01-029

 4-13-00
Reviewed by

 4-13-00
Concur

4/13/00

Battelle PNNL/RPG/Inorganic Analysis ...

ICPAES Data Report

Spent ion exchange resin sample **SL-644-SR** (RPL# 00-01367) and process blank was prepared using a wet-ash procedure prior to ICPAES and ICP-MS analysis. About 1.1532g of oven dried (95° C) spent ion exchange resin was processed using nitric acid and hydrogen peroxide in glass beakers and diluted to a final volume of 20ml. See attached sample processing flow diagram and description of wet-ash procedure below.

Spent ion exchange resin sample **SL-639-SR** (RPL# 00-01368) and process blank was prepared using a dry-ash procedure prior to ICPAES and ICP-MS analysis. About 1.2251g of oven dried (95° C) spent ion exchange resin was processed using nitric acid in glass scintillation vials and diluted to a final volume of 20ml. . See attached sample processing flow diagram and description of dry-ash procedure below.

Wet-ash procedure:

The spent ion exchange resin sample **SL-644-SR** was transferred from the 20cc scintillation vial that it was dried in, to a 250-ml glass beaker using about 25ml of water and several 1ml aliquots of 16M nitric acid. After the sample was transferred to the beaker a watch glass was placed on the beaker and the beaker placed on a small 4" x 6" Corning hot plate (temp. knob set to about "3"). As soon as the mixture got hot (90 to 120°C), dark orange colored NO_x fumes and foam appeared. A separate process blank was prepared similarly to the sample. All reagents used on the sample were included in the process blank. The sample and a process blank were brought to a rapid boil and allowed to evaporate over a period of about two hours. When the sample and acid evaporated to near dryness, dark orange fumes again began to appear. Small one to two ml aliquots of 16M HNO₃ were added to the boiling mixture over a half-hour time period. Since no additional dark orange fumes appeared, 0.25ml of 30% hydrogen peroxide was added to the hot mixture. A vigorous reaction began along with foaming in the glass beaker in which the foam went about one-third the way up the wall. Several additional aliquots (0.25ml) of hydrogen peroxide were added. Shortly afterward the foam subsided the mixture was allowed to evaporate to near dryness. Foam was still present when the mixture was near dryness. About 0.25ml of hydrogen peroxide was added at this time. As soon as the peroxide contacted the mixture a rapid reaction occurred in which the residue in the beaker turned from an orange-yellow color to a dark mixture of fine black particles like carbon. Ten ml of 16M nitric acid was immediately added to the mixture and the hot plate temperature reduced to "low" position. The heated mixture continuously produced small bubbles and after about 15 minutes some clearing could be seen. The mixture was allowed to remain on the hot plate set at "low" over night. The next morning the mixture had evaporated to near dryness with a very small amount of dark particles remaining. About 0.4ml of 16M nitric acid and 18.6ml of water was added to the sample and blank and warmed on the hot plate for about 10 minutes on "low" setting. The process blank and sample was allowed to cool to room temperature then filtered using a 47mm diameter 0.45µm nitrocellulose membrane filter. Ten ml of process blank and sample filtrate

4/13/00

Battelle PNNL/RPG/Inorganic Analysis ... ICPAES Data Report

was placed in separate pre-cleaned and labeled scintillation vials marked for ICP-MS analysis. Similarly, the remaining filtered process blank and sample was placed in pre-cleaned and labeled scintillation vials marked for ICPAES analysis. Because the samples were prepared in glass beakers, boron, silicon and sodium are likely to present in both the blank and sample solutions.

Dry-ash procedure:

The spent ion exchange resin sample **SL-639-SR** was processed in the same 20cc glass scintillation vial that was used for drying the resin. The glass scintillation vial containing the oven-dried resin sample was placed inside a 100-ml glass beaker with a watch glass on top of the beaker. A second pre-cleaned, glass scintillation vial, used for the process blank, was placed inside a 100ml glass beaker with a watch glass on top of the beaker. Both beakers with sample and process blank vials were placed in a cold (room temperature) programmable muffle furnace. The muffle furnace temperature ramp-rate, hold-temperature and hold-time was programmed as follows. The dry cycle was set for a ramp-rate of 10°C/minute; hold-temperature of 130°C; and hold-time of 1 hour. The ash cycle was set for a ramp-rate of 10°C/minute; hold-temperature of 450°C; and hold-time of 10 hours. After the furnace cooled to about 100°C the beakers with vials were removed and set aside to cool to room temperature. Only a small amount of gray-ash (less than approximately 50mg) remained in the vial that originally held the resin. About 5ml of 16M nitric acid was added to the ash residue and also process blank scintillation vials (scintillation vials still in 100ml beakers). The 100ml beakers with sample and process blank vials place on a small 4" x 6" Corning hot plate set to about 120°C. The sample and process blank liquid was allowed to evaporate to about 0.5ml. The hot plate temperature was reduced to about 70 to 90°C and about 10ml of water was added and allowed to continue heating for about 20 minutes. The sample and blank solutions were removed from the hot plate and allowed to cool to room temperature. Water was added to bring the final volume to 20ml. The entire sample appeared to be dissolved. No noticeable residue remained after diluting to volume. The final solutions were approximately 0.3M in nitric acid. Ten ml of sample and blank were transferred to separate pre-cleaned scintillation vials labeled for ICP-MS analysis. The remaining 10ml of sample and process blank was labeled for ICPAES analysis. Because the samples were prepared in 20cc glass scintillation vials, boron, silicon and sodium are likely to present in both the blank and sample solutions.

Analytes of interest include: Al, Ag, Ba, Ca, Cd, Cr, Cu, Fe, K, La, Mg, Mn, Na, Ni, Pb, Ti, and Zn. Reference, Table 1 "Analysis of Dissolved Ion Exchange Resins". MRQ's for all analytes of interest were met. Many of the analytes of interest were detected in both resin samples. Sample **SL-644-SR** generally had higher concentrations of similar analytes than sample **SL-639-SR**. All ICPAES measurement results are reported in µg/g dry weight of spent ion exchange resin and have been corrected for processing and analytical dilution.

4/13/00

Battelle PNNL/RPG/Inorganic Analysis ... ICPAES Data Report

Quality control check-standard results met tolerance requirements for all analytes except as noted below. Following is a list of quality control measurement results relative to ICPAES analysis tolerance requirements

Five fold serial dilution:

(Solid samples)

Results were within tolerance limit of $\leq 10\%$ for all analytes tested after correcting for dilution except for nickel in sample SL-644-SR. Nickel concentration after dilution correction was slightly above the 10% limit (10.7%). Other analyte results above EQL were well within tolerance limit. The reason for the slightly high result is not known.

Duplicate RPD (Relative Percent Difference):

(Solid samples)

Duplicate RPD was not tested because of limit sample material available.

Post-Spiked Samples (Group A):

(Solid samples)

All analytes of interest were recovered within tolerance limit of 75% to 125%.

Post-Spiked Samples (Group B):

(Solid samples)

All analytes of interest were recovered within tolerance of 75% to 125%.

Blank Spike:

(Solid samples)

A blank spike was not prepared.

Matrix Spiked Sample:

(Solid samples)

A matrix spike is was not prepared due to insufficient sample material.

Quality Control Check Standards (solid samples):

Concentration of all analytes of interest was within tolerance limit of $\pm 10\%$ accuracy in standards: QC_MCVA, QC_MCVB, and QC_SSTMV. Calibration Blank (ICP98.0) concentration was acceptable, less than two times IDL.

High Calibration Standard Check (solid samples):

Verification of the high-end calibration for all analytes was within tolerance limits of $\pm 5\%$ accuracy.

4/13/00

Battelle PNNL/RPG/Inorganic Analysis ... ICPAES Data Report

Process Blank: (solid samples)

All analytes of interest were within tolerance limit of \leq EQL or $< 5\%$ of sample concentration in the prepared samples. Sodium was the only analyte of interest measured in the process blank that was above EQL (16.3 ug/g). However, sodium in the process blank was less than 2% of the concentration in sample **SL-639-SR** and less than 0.1% of the concentration in sample **SL-644-SR**.

Laboratory Control Standard (LCS):

(Solid samples) An LCS sample was not prepared.

Please note bracketed values listed in the data report are within ten times instrument detection limit and have a potential uncertainty much greater than 15%.

Comments:

- 1) "Final Results" have been corrected for all laboratory dilution performed on the sample during processing and analysis unless specifically noted.
- 2) Detection limits (DL) shown are for acidified water. Detection limits for other matrices may be determined if requested.
- 3) Routine precision and bias is typically $\pm 15\%$ or better for samples in dilute, acidified water (e.g. 2% v/v HNO₃ or less) at analyte concentrations greater than ten times detection limit up to the upper calibration level. This also presumes that the total dissolved solids concentration in the sample is less than 5000 $\mu\text{g/mL}$ (0.5 per cent by weight).
- 4) Absolute precision, bias and detection limits may be determined on each sample if required by the client.
- 5) The maximum number of significant figures for all ICP measurements is 2.

4/13/00

Multiplier= RPL/LAB #=		17.3 00-1367-PB	17.3 00-1367	16.3 00-1368-PB	16.3 00-1368		
Client ID= Run Date=		SL-644-SR Process Blank (Wet- Ashed) 3/15/00	SL-644-SR (Wet- Ashed) 3/15/00	SL-639-SR Process Blank (Dry- Ashed) 3/15/00	SL-639-SR (Dry-Ashed) 3/15/00		
Det. Limit (ug/mL)	(Analyte)	ug/g	ug/g	ug/g	ug/g		
0.015	Ag	--	5.04	--	--	--	--
0.060	Al	[2.8]	60.9	[1.00]	[6.5]	--	--
0.080	As	--	--	--	[1.9]	--	--
0.050	B	39.8	169	26.7	89.9	--	--
0.010	Ba	--	[0.58]	--	[0.41]	--	--
0.005	Be	--	--	--	--	--	--
0.100	Bi	--	[9.8]	--	--	--	--
0.250	Ca	[17]	147	--	[9.9]	--	--
0.015	Cd	--	[0.56]	--	--	--	--
0.100	Ce	--	--	--	--	--	--
0.025	Co	--	70.9	--	--	--	--
0.020	Cr	--	669	--	5.00	--	--
0.015	Cu	--	116	--	[1.1]	--	--
0.050	Dy	--	--	--	--	--	--
0.100	Eu	--	--	--	--	--	--
0.025	Fe	[2.3]	84.2	--	30.4	--	--
2.000	K	--	[220]	--	[160]	--	--
0.025	La	--	--	--	--	--	--
0.020	Li	--	--	--	--	--	--
0.100	Mg	[2.8]	[5.7]	--	[6.2]	--	--
0.005	Mn	--	0.922	--	1.63	--	--
0.030	Mo	--	--	--	--	--	--
0.100	Na	71.3	83,800	41.3	2,300	--	--
0.100	Nd	--	--	--	--	--	--
0.030	Ni	[1.3]	51.5	[1.5]	[4.4]	--	--
0.100	P	--	[9.1]	--	[6.4]	--	--
0.060	Pb	--	10.9	--	--	--	--
0.300	Pd	--	--	--	[6.9]	--	--
0.300	Rh	--	--	--	--	--	--
0.075	Ru	--	[1.4]	--	--	--	--
0.050	Sb	--	--	--	--	--	--
0.050	Se	--	--	--	--	--	--
0.100	Si	19.9	22.8	[2.6]	39.7	--	--
1.000	Sn	--	--	--	--	--	--
0.005	Sr	--	1.57	--	2.42	--	--
0.500	Te	--	--	--	--	--	--
0.800	Th	--	[14]	--	--	--	--
0.005	Ti	--	4.02	--	[0.15]	--	--
0.250	Tl	--	--	--	--	--	--
2.000	U	--	--	--	--	--	--
0.015	V	--	--	--	--	--	--
0.500	W	--	--	--	--	--	--
0.010	Y	--	--	--	--	--	--
0.020	Zn	[0.90]	20.6	--	[0.45]	--	--
0.025	Zr	--	181	--	--	--	--

Note: 1) Overall error greater than 10-times detection limit is estimated to be within +/- 15%.

2) Values in brackets [] are within 10-times detection limit with errors likely to exceed 15%.

3) "--" indicate measurement is below detection. Sample detection limit may be found by multiplying "det. limit" (far left column) by "multiplier" (top of each column).

WO/Project: W45529/29953
Client: D. Kurath

ACL Numbers: 00-01367 & 00-01368
ASR Number 5732

Procedure: PNNL-ALO-131, "Mercury Digestion"
PNNL-ALO-201, "Mercury Analysis"

Analyst: J. J. Wagner

Digestion Date: March 14, 2000 Analysis Date: March 15, 2000

M&TE: Hg system (WD14126); Mettler AT400 Balance (360-06-01-029) See Chemical Measurement Center 98620 RIDS for Hg File for Calibration, Standards Preparations, and Maintenance Records.

Analyst: Jerry L. Wagner 3-30-00
Approval: [Signature] Date 3-30-00

Final Results:

The samples were analyzed by cold vapor atomic absorption spectrophotometry for inorganic mercury as specified in ASR 5732. Approximately 0.1g dry sample weight was processed and diluted to a final volume of 25ml per procedure ALO-131. No additional dilution was performed. The mercury concentration results are presented in the table below.

Lab ID	Solid Sample ID	Solids Grams	Solids Dig Fctr	Solids Anal Fctr	Hg ug/g	RPD (%)
PB-1	Reagent Process Blank	0.0997	251	1	0.193	
PB-2	Reagent Process Blank	0.0997	251	1	0.115	
00-01367	SL-644-Hg-1	0.0836	299	1	0.22	
00-01367D	SL-644-Hg-2	0.1030	243	1	0.23	3
00-01368	SL-639-Hg-1	0.1051	238	1	0.10	
00-01368D	SL-639-Hg-2	0.1071	233	1	0.16	N/A

RPD = Relative Percent Difference (between sample and duplicate/replicate)
 "Sample weight" used for the process blank is an average weight of the samples.
 N/A = RPD is not calculated when results are less than 5 x IDL

Notes:

- 1) "Final Results" have been corrected for all dilution performed on the sample during processing or analysis.
- 2) The low calibration standard is defined as the estimated detection limit (IDL) for the reported results and assumes non-complex aqueous matrices. Actual detection limits or quantitation limits for specific sample matrices may be determined, if requested.
- 3) Routine precision and bias is typically $\pm 15\%$ or better for non-complex aqueous samples that are free of interference.

Q.C. Comments:

Following are results of quality control checks performed during Hg analyses. In general, quality control checks met the requirements of the governing QA Plan.

Working Blank Spike/Process Blank Spike: Process Blank Spike recovery is 96% and 95%, well within the acceptance criteria of 80% to 120%.

Matrix Spiked Sample: A matrix spike was prepared for the samples submitted under this ASR. However, recovery of the matrix spike (27%) fell below the acceptance criteria of 75% to 125%. The high carbon content in the resin may have caused failure of the matrix spike by requiring more oxidizing reagent than was available. Recovery of a post-spike for that sample was 105%, well within the acceptance criteria of 75% to 125%. Since the post-spike recovery was acceptable it also implies that low recovery of the matrix spike was related to sample digestion.

Duplicate: Relative percent difference for the duplicate samples is within acceptance criteria of $\leq 20\%$ RPD for RPL# 00-01367 and 00-1367D (3% RPD).

Laboratory Control Sample (solids): Sample recovery of mercury in SRM-2709 San Joaquin Valley Soil certified by NIST to contain 1.40 ± 0.08 $\mu\text{g/g}$ was recovered within acceptance criteria of 75% to 125%.

System Blank/Processing Blanks: A system blank was process during the analysis of the sample. The concentration measured was within about two times detection limit or less. Some samples were about the same concentration as the process blank and other samples were many times this level.

Quality Control Calibration Verification Check Standards: Six mid-range verification standards were analyzed throughout the analysis run. All were within the acceptance criteria of 80% to 120% recovery for the verification standard.



Pacific Northwest Laboratories

Project Number

Internal Distribution

Date April 7, 2000

To Dean Kurath

From Tom Farmer *C. J. Farmer 7 Apr 00*

Subject ICP/MS Analysis of Submitted Samples
(ALO#00-001367 and 00-001368)

329/4 File
LSO Project File
Jerry Wagner

Pursuant to your request, the 4 samples that you submitted for analysis were analyzed by ICPMS for selected elements. The results of this analysis are reported on the attached pages. Both the method detection limit values, as listed on ASR #5732, and the ICP/MS analyzed values have been provided.

Single element CPI standards for V, As, Sn, Ti and Se, an NIST uranium standard (4321B), an Amersham ^{99}Tc standard, Isotope Products standards for ^{129}I , ^{239}Pu , ^{233}U , ^{242}Pu , ^{241}Am , ^{243}Am and ^{237}Np and an ^{127}I standard, prepared from Fisher potassium iodide (LOT# 35260) were used to generate the calibration curves. Independent standards of each element were used as the continuing calibration verification (CCV) standards.

The ^{99}Tc values reported assume that the Ru present is exclusively fission-product Ru, and therefore does not have an isotope at m/z 99; i.e., everything observed at m/z 99 is due to ^{99}Tc . The fingerprint we're seeing for Ru is obviously not natural, and is consistent with that observed in previous tank waste analyses.

Interference corrections were performed on ^{129}I (xenon corrected), ^{239}Pu (uranium hydride corrected), ^{126}Sn (tellurium and xenon corrected).

Values for the following isotopes were obtained using responses from related isotopes: ^{240}Pu (obtained from ^{239}Pu), AMU-241, 243 were obtained from ^{241}Am and ^{243}Am and AMU-242 was obtained from ^{242}Pu .

If you have any questions regarding this analysis, feel free to call me at 372-0700 or James Bramson at 372-0624



*proj 29953
T2.10.4
Tosh 10*

Dean Kurath Analysis

April 7, 2000

J.B. Brown
4/17/00

Sample ID	Client ID	ICP/MS Number	MRQ ⁽¹⁾ Vanadium MDL Analyzed $\mu\text{g/g}$	MRQ ⁽¹⁾ Arsenic MDL Analyzed $\mu\text{g/g}$	MRQ ⁽¹⁾ Selenium MDL Analyzed $\mu\text{g/g}$	MRQ ⁽¹⁾ Tc-99 MDL Analyzed $\mu\text{g/g}$
1% HNO ₃		00330b1	<0.05	<0.1	<0.8	<0.05
1% HNO ₃		00330b6	<0.05	<0.1	<0.8	<0.05
1% HNO ₃		00330b29	<0.05	<0.1	<0.8	0.18 \pm 0.04
00-001367-PB	Process Blank	00330b7	<6.0	<2.3	<20	<2
00-001368-PB	Process Blank	00330b8	<6.0	<2.3	<20	<2
00-001367	SL-644-SR	00330b10&26	<6.0	<2.3	<20	<2
00-001367 Dup	SL-644-SR	00330b11&28	<6.0	<2.3	<20	<2
00-001368	SL-639-SR	00330b9&23	<6.0	<2.3	<20	<2
00-001368 + spike	SL-639-SR	00330b12&27	<6.0	<2.3	<20	<2
Spike Recovery			98%	102%	81%	93%
1ppb Se		00330b19			0.86 \pm 0.21	
2ppb Se		00330b30			2.0 \pm 0.2	
5ppb Tc-99		00330b4				5.07 \pm 0.04
5ppb Tc-99		00330b15				5.12 \pm 0.01
500ppb Co		00330b33				0.18 \pm 0.08
0.5ppb V, As		00330b19	0.506 \pm 0.018	0.43 \pm 0.06		
2ppb V, As		00330b30	1.93 \pm 0.06	1.9 \pm 0.3		
0.5ppb I-127		00331a3				
1ppb I-127		00331a17				
0.1ppb I-129		00331a2				
0.1ppb I-129		00331a14				
2ppb Ti		00403a9				
2ppb Ti		00403a27				
0.05ppb Np-237, Pu-239		00403a12				
0.5ppb Np-237, Pu-239		00403a26				
Multi CCV		00403a16				
True Value						
Multi CCV		00403a31				
True Value						
U030		00403a4				
U030		00403a27				
True Value						
0.1ppb U-233		00403a12				
0.1ppb U-233		00403a26				
U-350 Atom %						
True Value						

DATA REVIEW

Reviewed: D.J. SarnowskiDate: 16 Apr 00 10/5(1) Minimum Reportable Amounts, note different units of $\mu\text{g/g}$

Dean Kurath Analysis

April 7, 2000

JCBanner
4/7/00

Sample ID	Client ID	ICP/MS Number	MRQ ^(U) Tl-126 MDL Analyzed µg/g ^(U) ng/g ± 1 SD	MRQ ^(U) I-127 MDL Analyzed µg/g ^(U) ng/g ± 1 SD	MRQ ^(U) I-129 MDL Analyzed µg/g ^(U) ng/g ± 1 SD	MRQ ^(U) Thallium MDL Analyzed µg/g ^(U) ng/g ± 1 SD
1% HNO3		00330b1	<0.06	<0.12	<0.031	<0.05
1% HNO3		00330b6	<0.06	<0.11	<0.028	<0.05
1% HNO3		00330b29	<0.06	<0.10	<0.028	<0.05
00-001367-PB	Process Blank	00330b7	<6.0	<30	<30	<6.0
00-001368-PB	Process Blank	00330b8	<6.0	<30	<30	<6.0
00-001367	SL-644-SR	00330b10&26	<6.0	19.4 ± 0.3	<30	<6.0
00-001367 Dup	SL-644-SR	00330b11&28	<6.0	21.3 ± 1.0	<30	<6.0
00-001368	SL-639-SR	00330b9&23	<6.0	<30	<30	<6.0
00-001368 + spike	SL-639-SR	00330b12&27	<6.0	68.5 ± 3.9	3.3 ± 0.9	<6.0
Spike Recovery				83%	26 ± 3	160 ± 7
1ppb Se		00330b19			84%	95%
2ppb Se		00330b30				
5ppb Tc-99		00330b4				
5ppb Tc-99		00330b15				
500ppb Co		00330b33				
0.5ppb V, As		00330b19				
2ppb V, As		00330b30				
0.5ppb I-127		00331a3		0.545 ± 0.012	0.11 ± 0.03	2.02 ± 0.11
1ppb I-127		00331a17		0.931 ± 0.057	0.085 ± 0.014	2.02 ± 0.10
0.1ppb I-129		00331a2				
0.1ppb I-129		00331a14				
2ppb Ti		00403a9				
2ppb Ti		00403a27				
0.05ppb Np-237, Pu-239		00403a12				
0.5ppb Np-237, Pu-239		00403a26				
Multi CCV		00403a16				
True Value		00403a31				
Multi CCV		00403a4				
True Value		00403a27				
U030						
U030						
True Value						
0.1ppb U-233		00403a12				
0.1ppb U-233		00403a26				
U-350 Atom %						
True Value						

DATA REVIEW

Reviewed by: *Q. J. Hanner*

Date: *4/29/00*

* Results are from procedure 00403a.
† Calculated from response of different isotope. Should be considered semiquantitative.

Dean Kurath Analysis

April 7, 2000

JPBrown
4/7/00

Sample ID	Client ID	ICPMS Number	MRQ ^(U) MDL Analyzed $\mu\text{g/g}^{(U)}$	*U-233 ng/g \pm 1 SD	MRQ ^(U) MDL Analyzed $\mu\text{g/g}^{(U)}$	*U-234 ng/g \pm 1 SD	MRQ ^(U) MDL Analyzed $\mu\text{g/g}^{(U)}$	*U-235 ng/g \pm 1 SD	MRQ ^(U) MDL Analyzed $\mu\text{g/g}^{(U)}$	*U-236 ng/g \pm 1 SD
1%HNO3		00330b1		<0.02		<0.01		<0.02		<0.02
1%HNO3		00330b6		<0.02		<0.01		<0.02		<0.02
1%HNO3		00330b29		<0.02		<0.01		<0.02		<0.02
00-001367-PB	Process Blank	00330b7	<0.6	<1.7	<6.0	<0.9	<6.0	<1.7	<6.0	<1.7
00-001368-PB	Process Blank	00330b8	<0.6	<1.6	<6.0	<0.8	<6.0	<1.6	<6.0	<1.6
00-001367	SL-644-SR	00330b10&26	<0.6	<5.8	<6.0	<2.9	<6.0	144 \pm 4	<6.0	16 \pm 2
00-001367 Dup	SL-644-SR	00330b11&28	<0.6	<5.2	<6.0	<2.6	<6.0	159 \pm 8	<6.0	14 \pm 2
00-001368	SL-639-SR	00330b9&23	<0.6	<2.0	<6.0	<1.0	<6.0	<2.0	<6.0	<2.0
00-001368 + spike	SL-639-SR	00330b12&27	<0.6	40.3 \pm 1.1						
Spike Recovery										
1ppb Se		00330b19								
2ppb Se		00330b30								
5ppb Tc-99		00330b4								
5ppb Tc-99		00330b15								
500ppb Co		00330b33								
0.5ppb V, As		00330b19								
2ppb V, As		00330b30								
0.5ppb I-127		00331a3								
1ppb I-127		00331a17								
0.1ppb I-129		00331a2								
0.1ppb I-129		00331a14								
2ppb Ti		00403a9								
2ppb Ti		00403a27								
0.05ppb Np-237, Pu-239		00403a12								
0.5ppb Np-237, Pu-239		00403a26								
Multi CCV		00403a16								
True Value		00403a31								
Multi CCV										
True Value										
U030		00403a4								
U030		00403a27								
True Value										
0.1ppb U-233		00403a12		0.095 \pm 0.012				0.306 \pm 0.020		
0.1ppb U-233		00403a26		0.091 \pm 0.016				0.282 \pm 0.004		
								0.307		
U-350 Atom %		00403a34								
True Value										
				Atom %	0.2536 \pm 0.1007	Atom %	35.264 \pm 0.200	Atom %	0.1826 \pm 0.0443	
					0.2498		35.190		0.1673	

DATA REVIEW

Reviewed by *D.J. Jones*Date: *7 Apr 00*

39

* Results are from procedure 00403a.

Dean Kurath Analysis

April 7, 2000

gpbrown
4/7/00

Sample ID	Client ID	ICP/MS Number	M&Q (U) MDL Analyzed μg/g (U) ± 1 SD	(M&Q (U)) *U-238 MDL Analyzed ng/g ± 1 SD	(M&Q (U)) *Np-237 MDL Analyzed ng/g ± 1 SD	(M&Q (U)) *Pu-239 MDL Analyzed μg/g (U) ± 1 SD	(M&Q (U)) *Pu-240 MDL Analyzed μg/g (U) ± 1 SD
1%HNO3		00330b1	<0.07	<0.07	<0.02	<0.02	<0.02
1%HNO3		00330b6	<0.07	<0.07	<0.02	<0.02	<0.02
1%HNO3		00330b29	<0.07	<0.07	<0.02	<0.02	<0.02
00-001367-PB	Process Blank	00330b7	<6.0	<6.1	<1.7	<1.7	<1.7
00-001368-PB	Process Blank	00330b8	<6.0	<5.7	<1.6	<1.6	<1.6
00-001367	SL-644-SR	00330b10&26	<6.0	14800 ± 400	45 ± 5	69 ± 10	15 ± 4
00-001367 Dup	SL-644-SR	00330b11&28	<6.0	14800 ± 200	48.6 ± 1.3	63.8 ± 4.6	13 ± 2
00-001368	SL-639-SR	00330b9&23	<6.0	21 ± 11	<2.2	<2.0	<2.0
00-001368 + spike	SL-639-SR	00330b12&27	<6.0	161 ± 5	36.7 ± 2.7	35.4 ± 1.6	<6.0
Spike Recovery							
1ppb Se		00330b19			85%	82%	
2ppb Se		00330b30					
5ppb Tc-99		00330b4					
5ppb Tc-99		00330b15					
500ppb Co		00330b33					
0.5ppb V, As		00330b19					
2ppb V, As		00330b30					
0.5ppb I-127		00331a3					
1ppb I-127		00331a17					
0.1ppb I-129		00331a2					
0.1ppb I-129		00331a14					
2ppb TI		00403a9					
2ppb TI		00403a27					
0.05ppb Np-237, Pu-239		00403a12			0.044 ± 0.008	0.0513 ± 0.008	
0.5ppb Np-237, Pu-239		00403a26			0.486 ± 0.029	0.515 ± 0.045	
Multi CCV		00403a16					
True Value							
Multi CCV		00403a31					
True Value							
U030		00403a4		9.79 ± 0.19			
U030		00403a27		9.51 ± 0.11			
True Value				9.75			
0.1ppb U-233		00403a12					
0.1ppb U-233		00403a26					
			Atom %				
U-350 Atom %			64.300 ± 0.218				
True Value			64.393				

DATA REVIEW

Review: O'Hanrahan
U-350 Apr 00
494

* Results are from procedure 00403a.

April 7, 2000

Dean Kurath Analysis

MAIN RESULTS

Faint: O. J. Tanner
 Dated: 7 Apr 1960

Dr. J. Z. A. P. P.

* Results are from procedure 00403a.

††AMU-242 calculated using Pu-242. AMU-241,243 calculated using Am-241, Am-243 results are from procedure 00-403a.

ICP-MS Analysis of SL-644 and SL-639 Spent Resin

April 7, 2000

Sample	Client ID	ICP/MS Number	Vanadium		Arsenic		Selenium		Tc-99	
			MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed $\text{ng/g} \pm 1 \text{ SD}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed $\text{ng/g} \pm 1 \text{ SD}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed $\text{ng/g} \pm 1 \text{ SD}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed $\text{ng/g} \pm 1 \text{ SD}$
1% HNO3		00330b1		<0.05		<0.1		<0.8		<0.05
1% HNO3		00330b6		<0.05		<0.1		<0.8		<0.05
1% HNO3		00330b29		<0.05		<0.1		<0.8		0.18 \pm 0.04
00-001367-PB	Process Blank	00330b7	<6.0	5.6 \pm 0.9	<2.3	<3.0	<20	<28	<2	<1.5
00-001368-PB	Process Blank	00330b8	<6.0	4.22 \pm 0.02	<2.3	<3.0	<20	<26	<2	<1.5
00-001367	SL-644-SR	00330b10&26	<6.0	96.8 \pm 2.9	<2.3	302 \pm 17	<20	<63	<2	6540 \pm 80
00-001367 Dup	SL-644-SR	00330b11&28	<6.0	90.0 \pm 2.5	<2.3	270 \pm 40	<20	<63	<2	6940 \pm 130
00-001367 average	SL-644-SR			93	11	286	33	<63	<7.3	6740
00-001368	SL-639-SR	00330b9&23	<6.0	13.6 \pm 0.3	<2.3	2130 \pm 90	1023	67 \pm 24	32	6950 \pm 50
00-001368 + spike	SL-639-SR	00330b12&27	<6.0	77.7 \pm 0.4	<2.3	2230 \pm 40	<20	120 \pm 40	<2	7560 \pm 80
Spike Recovery				98%		102%		81%		93%
1ppb Se		00330b19						0.86 \pm 0.21		
2ppb Se		00330b30						2.0 \pm 0.2		
5ppb Tc-99		00330b4								5.07 \pm 0.04
5ppb Tc-99		00330b15								5.12 \pm 0.01
500ppb Co		00330b33								0.18 \pm 0.08
0.5ppb V, As		00330b19		0.506 \pm 0.018		0.43 \pm 0.06				
2ppb V, As		00330b30		1.93 \pm 0.06		1.9 \pm 0.3				
0.5ppb I-127		00331a3								
1ppb I-127		00331a17								
0.1ppb I-129		00331a2								
0.1ppb I-129		00331a14								
2ppb Ti		00403a9								
2ppb Ti		00403a27								
0.05ppb Np-237, Pu-239		00403a12								
0.5ppb Np-237, Pu-239		00403a26								
Multi CCV		00403a16								
True Value										
Multi CCV		00403a31								
True Value										
U030		00403a4								
U030		00403a27								
True Value										
0.1ppb U-233		00403a12								
0.1ppb U-233		00403a26								

U-350 Atom %

True Value

(1) MRQ = BNFL specified minimum reportable quantity. Note that the MRQ units are in $\mu\text{g/g}$ while analyte results are in ng/g .

(2) Concentration based on volume of resin subsample

April 7, 2000

(1) MRQ = BNFL specified minimum reportable quantity. Note that the MRQ units are in ug/g while analyte results are in ng/g.
(2) Concentration based on volume of resin subsample

True Value

- Results are from procedure 00331a.

ICP-MS Analysis of SL-644 and SL-639 Spent Resin

April 7, 2000

Sample ID	Client ID	ICP/MS Number	*U-233			*U-234			*U-235			*U-236		
			MRQ ⁽¹⁾ $\mu\text{g/g}$	MRQ ⁽¹⁾ Analyzed ng/g	$\pm 1 \text{ SD ng/mL}^{(2)}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	MRQ ⁽¹⁾ Analyzed ng/g	$\pm 1 \text{ SD ng/mL}^{(2)}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	MRQ ⁽¹⁾ Analyzed ng/g	$\pm 1 \text{ SD ng/mL}^{(2)}$	MRQ ⁽¹⁾ $\mu\text{g/g}$	MRQ ⁽¹⁾ Analyzed ng/g	$\pm 1 \text{ SD ng/mL}^{(2)}$
1%HNO3		00330b1		<0.02			<0.01			<0.02			<0.02	
1%HNO3		00330b6		<0.02			<0.01			<0.02			<0.02	
1%HNO3		00330b29		<0.02			<0.01			<0.02			<0.02	
00-001367-PB	Process Blank	00330b7	<0.6	<1.7		<6.0	<0.9		<6.0	<1.7		<6.0	<1.7	
00-001368-PB	Process Blank	00330b8	<0.6	<1.6		<6.0	<0.8		<6.0	<1.6		<6.0	<1.6	
00-001367	SL-644-SR	00330b10&26	<0.6	<5.8		<6.0	<2.9		<6.0	144 ± 4		<6.0	16 ± 2	
00-001367 Dup	SL-644-SR	00330b11&28	<0.6	<5.2		<6.0	<2.6		<6.0	159 ± 8		<6.0	14 ± 2	
00-001367 average				<5.2	<0.6		<2.6			152	17		15	2
00-001368	SL-639-SR	00330b9&23	<0.6	<2.0	<1	<6.0	<1.0	<0.5	<6.0	<2.0	<1	<6.0	<2.0	<1
00-001368 + spike	SL-639-SR	00330b12&27	<0.6	40.3 ± 1.1										
Spike Recovery			94%											
1ppb Se		00330b19												
2ppb Se		00330b30												
5ppb Tc-99		00330b4												
5ppb Tc-99		00330b15												
500ppb Co		00330b33												
0.5ppb V, As		00330b19												
2ppb V, As		00330b30												
0.5ppb I-127		00331a3												
1ppb I-127		00331a17												
0.1ppb I-129		00331a2												
0.1ppb I-129		00331a14												
2ppb Tl		00403a9												
2ppb Tl		00403a27												
0.05ppb Np-237, Pu-239		00403a12												
0.5ppb Np-237, Pu-239		00403a26												
Multi CCV		00403a16												
True Value		00403a31												
Multi CCV														
True Value														
U030		00403a4												
U030		00403a27												
True Value														
0.1ppb U-233		00403a12	0.095 ± 0.012						0.306 ± 0.020			0.1826 ± 0.0443		
0.1ppb U-233		00403a26	0.091 ± 0.016						0.282 ± 0.004			0.1673		
U-350 Atom %		00403a34				Atom %			Atom %			Atom %		
True Value						0.2536 ± 0.1007			35.264 ± 0.200			0.1826 ± 0.0443		
						0.2498			35.190			0.1673		

ICP-MS Analysis of SL-644 and SL-639 Spent Resin

April 7, 2000

Sample ID	Client ID	ICP/MS Number	*U-238		*Np-237		*Pu-239		*Pu-240	
			MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed ng/g \pm 1 SD ng/mL ⁽²⁾	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed ng/g \pm 1 SD ng/mL ⁽²⁾	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed ng/g \pm 1 SD ng/mL ⁽²⁾	MRQ ⁽¹⁾ $\mu\text{g/g}$	Analyzed ng/g \pm 1 SD ng/mL ⁽²⁾
1% HNO3		00330b1		<0.07		<0.02		<0.02		<0.02
1% HNO3		00330b6		<0.07		<0.02		<0.02		<0.02
1% HNO3		00330b29		<0.07		<0.02		<0.02		<0.02
00-001367-PB	Process Blank	00330b7	<6.0	<6.1	<6.0	<1.7	<6.0	<1.7	<6.0	<1.7
00-001368-PB	Process Blank	00330b8	<6.0	<5.7	<6.0	<1.6	<6.0	<1.6	<6.0	<1.6
00-001367	SL-644-SR	00330b10&26	<6.0	14800 \pm 400	<6.0	45 \pm 5	<6.0	69 \pm 10	<6.0	15 \pm 4
00-001367 Dup	SL-644-SR	00330b11&28	<6.0	14800 \pm 200	<6.0	48.6 \pm 1.3	<6.0	63.8 \pm 4.6	<6.0	13 \pm 2
00-001367 average		1707		14800		47	5	66		14
00-001368	SL-639-SR	00330b9&23	<6.0	21 \pm 11	<6.0	<2.2	<1.1	<2.0	<6.0	<2.0
00-001368 + spike	SL-639-SR	00330b12&27		161 \pm 5	<6.0	36.7 \pm 2.7	<6.0	35.4 \pm 1.6	<6.0	<1
Spike Recovery				86%		85%		82%		2
1ppb Se		00330b19								
2ppb Se		00330b30								
5ppb Tc-99		00330b4								
5ppb Tc-99		00330b15								
500ppb Co		00330b33								
0.5ppb V, As		00330b19								
2ppb V, As		00330b30								
0.5ppb I-127		00331a3								
1ppb I-127		00331a17								
0.1ppb I-129		00331a2								
0.1ppb I-129		00331a14								
2ppb Ti		00403a9								
2ppb Ti		00403a27								
0.05ppb Np-237, Pu-239		00403a12								
0.5ppb Np-237, Pu-239		00403a26								
Multi CCV		00403a16								
True Value										
Multi CCV		00403a31								
True Value										
U030		00403a4		9.79 \pm 0.19						
U030		00403a27		9.51 \pm 0.11						
True Value				9.75						
0.1ppb U-233		00403a12								
0.1ppb U-233		00403a26								
U-350 Atom %				Atom %						
True Value				64.300 \pm 0.218						
				64.393						

* Results are from procedure 00403a.

(1) MRQ = BNFL specified minimum reportable quantity. Note that the MRQ units are in ug/g while analyte results are in ng/g.

(2) Concentration based on volume of resin subsample

ICP-MS Analysis of SL-644 and SL-639 Spent Resin

April 7, 2000

Sample ID	Client ID	ICP/MS Number	*††AMU-241		*††AMU-242		*††AMU-243	
			Analyzed ng/g	± 1 SD ng/mL ⁽²⁾	Analyzed ng/g	± 1 SD ng/mL ⁽²⁾	Analyzed ng/g	± 1 SD ng/mL ⁽²⁾
1% HNO ₃		00330b1	<0.02		<0.02		<0.02	
1% HNO ₃		00330b6	<0.02		<0.02		<0.02	
1% HNO ₃		00330b29	<0.02		<0.02		<0.02	
00-001367-PB	Process Blank	00330b7	<1.7		<1.7		<1.7	
00-001368-PB	Process Blank	00330b8	<1.6		<1.6		<1.6	
00-001367	SL-644-SR	00330b10&26	<5.8		<5.8		<5.8	
00-001367 Dup	SL-644-SR	00330b11&28	<5.2		<5.2		<5.2	
00-001367 average			<5.2	<0.6	<5.2	<0.6	<5.2	<0.6
00-001368	SL-639-SR	00330b9&23	<2.0	<1	<2.0	<1	<2.0	<1
00-001368 + spike	SL-639-SR	00330b12&27	4.85 ± 0.44		5.5 ± 2.4		13.5 ± 1.1	
Spike Recovery			115%		81%		98%	
1ppb Se		00330b19						
2ppb Se		00330b30						
5ppb Tc-99		00330b4						
5ppb Tc-99		00330b15						
500ppb Co		00330b33						
0.5ppb V, As		00330b19						
2ppb V, As		00330b30						
0.5ppb I-127		00331a3						
1ppb I-127		00331a17						
0.1ppb I-129		00331a2						
0.1ppb I-129		00331a14						
2ppb Ti		00403a9						
2ppb Ti		00403a27						
0.05ppb Np-237, Pu-239		00403a12						
0.5ppb Np-237, Pu-239		00403a26						
Multi CCV		00403a16	0.050 ± 0.005		0.105 ± 0.006		0.168 ± 0.009	
True Value			0.0516		0.106		0.144	
Multi CCV		00403a31	0.064 ± 0.007		0.116 ± 0.016		0.235 ± 0.011	
True Value			0.0688		0.106		0.191	
U030		00403a4						
U030		00403a27						
True Value								
0.1ppb U-233		00403a12						
0.1ppb U-233		00403a26						
U-350 Atom %								
True Value								

* Results are from procedure 00403a.
††AMU-242 calculated using Pu-242. AMU-241,243 calculated using Am-241, Am-243

(2) Concentration based on volume of resin subsample

preparation of resin samples for GEA, ICP-AES, ICP-MS

	vial tare	vial+resin	wet resin	dry resin @ 95 C (1)	dry resin @ 95 C (2)
	g	g	g	g	g
SL-639-SR	16.7666	19.6987	2.9321	1.2384	1.2251
SL-644-SR	16.9471	26.9733	10.0262	1.1659	1.1532
SL-639 density @ 95 C =		0.48	g/mL		
estimated volume of SL-639 sample =			2.55	mL	

- 1) This mass is determined by subtracting the tare weight of the vial from the mass of the vial + dry resin.
- 2) This mass is determined by subtracting the water loss from the original sample mass. The discrepancy appears to be due to the addition of a small radiation sticker. This mass is therefore the mass used in calculations.

liquid samples	vial tare	vial + liquid	liquid
	g	g	g
SL-639-LQ	16.6399	18.5687	1.9288
SL-644-LQ	16.7476	26.3832	9.6356

preparation of resin samples for Hg analyses

F factors	vial tare	vial+resin	damp resin	water loss	dry resin @ 95 C	F factor
	g	g	g	g	g	
SL-639-F	18.8105	19.4884	0.6779	0.008	0.6699	0.988
SL-644-F	18.7253	18.8954	0.1701	0.03	0.1401	0.824
	vial tare	vial+resin	wet resin	dry resin @ 95 C		
	g	g	g	g		
SL-639-Hg-1	25.5936	25.7	0.1064	0.1051		
SL-639-Hg-2	25.8151	25.9235	0.1084	0.1071		
SL-644-Hg-1	25.9315	26.033	0.1015	0.0836		
SL-644-Hg-2	25.6402	25.7652	0.125	0.1030		
SL-644-Hg-3	25.745	25.8708	0.1258	0.1036		

Radionuclide concentrations based on sample volume											
	Co-60 uCi/mL	Sb-125 uCi/mL	Cs-134 uCi/mL	Cs-137 uCi/mL	CePr-144 uCi/mL	Eu-154 uCi/mL	Eu-155 uCi/mL	Am-241 uCi/mL	Y-88 uCi/mL	Tc-95 uCi/mL	Tc-95 M uCi/mL
00-1367											
SL-644-SR (1)	1.51E-01	<3.E-3	1.89E-03	2.46E+00	<4.E-3	7.60E-04	1.65E-03	1.03E-03			
00-1368											
SL-639-SR (2)	1.66E-04	<1.6E-4	<3.5E-5	3.60E-05	<4E-4	9.25E-04	8.78E-04	5.13E-04	5.84E-05	1.27E-02	2.68E-01
00-1369											
SL-644-LQ (1)	8.22E-03	4.98E-05	2.31E-04	1.61E-02	6.05E-05	1.36E-04	9.34E-05	2.35E-04			
644 LQ:SR	5.44%		12.22%	0.65%		17.89%	5.66%	22.82%			
00-1370											
SL-639-LQ (3)	<6.E-6	<2.E-5	<6.E-6	<7.E-6	<4.E-5	6.32E-05	3.70E-05	3.43E-05		2.11E-05	3.45E-04
639 LQ:SR						8.54%	5.27%	8.35%		0.21%	0.16%
1) values based on an assumed 10 mL sample volume											
2) values based on a sample volume of 2.55 mL, estimated with the resin dry mass and density at 95 °C.											
3) values based on a 2 mL sample volume											
Radionuclide concentrations based on sample mass											
	Co-60 uCi/g	Sb-125 uCi/g	Cs-134 uCi/g	Cs-137 uCi/g	CePr-144 uCi/g	Eu-154 uCi/g	Eu-155 uCi/g	Am-241 uCi/g	Y-88 uCi/g	Tc-95 uCi/g	Tc-95 M uCi/g
00-1367											
SL-644-SR (1)	1.31E+00	<2.6E-2	1.64E-02	2.13E+01	<3.5E-2	6.59E-03	1.43E-02	8.93E-03			
00-1368											
SL-639-SR (1)	3.45E-04	<3.3E-4	<7.4E-5	7.50E-05	<8E-4	1.93E-03	1.83E-03	1.07E-03	1.22E-04	2.64E-02	5.58E-01
00-1369											
SL-644-LQ (2)	8.53E-03	5.17E-05	2.40E-04	1.67E-02	6.28E-05	1.41E-04	9.69E-05	2.44E-04			
00-1370											
SL-639-LQ (2)	<6.E-6	<2.E-5	<6.E-6	<7.E-6	<4.E-5	6.55E-05	3.84E-05	3.56E-05		2.19E-05	3.58E-04
1) Values based on dried sample mass at 95 °C. Includes contribution from interstitial liquid.											
2) Values based on sample mass (not dried). Density should be close to 1 as solution was water or very dilute caustic.											

Multiplier=		17.2	17.2			16.1	16.1		
RPL/LAB #=		00-1367-PB	00-1367		resin mass	00-1368-PB	00-1368		resin mass
Client ID=		SL-644-SR Process Blank (Wet- Ashed)	SL-644-SR (Wet- Ashed)		1.1532	SL-639-SR Process Blank (Dry- Ashed)	SL-639-SR (Dry-Ashed)		1.2251
Det. Limit	Run Date=	3/15/00	3/15/00	detect limit		3/15/00	3/15/00	detect limit	
(ug/mL)	(Analyte)	ug/g	ug/g	ug/g	ug/mL	ug/g	ug/g	ug/g	ug/mL
0.015	Ag	--	5.03	0.26	0.58	--	--	0.24	--
0.060	Al	[2.8]	60.9	1.03	7.0	[0.99]	[6.5]	0.97	[3.1]
0.080	As	--	--	1.37	--	--	[1.9]	1.29	[0.9]
0.050	B	39.4	170	0.86	20	26.4	89.9	0.81	43.2
0.010	Ba	--	[0.59]	0.17	[0.07]	--	[0.40]	0.16	[0.19]
0.005	Be	--	--	0.09	--	--	--	0.08	--
0.100	Bi	--	[9.8]	1.72	[1.1]	--	--	1.61	--
0.250	Ca	[17]	148	4.29	17	--	[9.9]	4.04	[4.8]
0.015	Cd	--	[0.56]	0.26	[0.06]	--	--	0.24	--
0.100	Ce	--	--	1.72	--	--	--	1.61	--
0.025	Co	--	70.9	0.43	8.2	--	--	0.40	--
0.020	Cr	--	669	0.34	77	--	4.99	0.32	2.40
0.015	Cu	--	116	0.26	13	--	[1.1]	0.24	[0.5]
0.050	Dy	--	--	0.86	--	--	--	0.81	--
0.100	Eu	--	--	1.72	--	--	--	1.61	--
0.025	Fe	[2.3]	84.2	0.43	9.7	--	30.4	0.40	14.6
2.000	K	--	[222]	34.31	[26]	--	[162]	32.30	[78]
0.025	La	--	--	0.43	--	--	--	0.40	--
0.020	Li	--	--	0.34	--	--	--	0.32	--
0.100	Mg	[2.8]	[5.8]	1.72	[0.7]	--	[6.2]	1.61	[3.0]
0.005	Mn	--	0.922	0.09	0.106	--	1.63	0.08	0.78
0.030	Mo	--	--	0.51	--	--	--	0.48	--
0.100	Na	70.5	83,813	1.72	9,665	40.8	2,295	1.61	1,102
0.100	Nd	--	--	1.72	--	--	--	1.61	--
0.030	Ni	[1.3]	51.5	0.51	5.9	[1.5]	[4.3]	0.48	[2.1]
0.100	P	--	[9.1]	1.72	[1.0]	--	[6.5]	1.61	[3.1]
0.060	Pb	--	10.9	1.03	1.3	--	--	0.97	--
0.300	Pd	--	--	5.15	--	--	[6.9]	4.84	[3.3]
0.300	Rh	--	--	5.15	--	--	--	4.84	--
0.075	Ru	--	[1.3]	1.29	[0.2]	--	--	1.21	--
0.050	Sb	--	--	0.86	--	--	--	0.81	--
0.050	Se	--	--	0.86	--	--	--	0.81	--
0.100	Si	19.7	22.8	1.72	2.6	[2.6]	39.7	1.61	19.1
1.000	Sn	--	--	17.15	--	--	--	16.15	--
0.005	Sr	--	1.57	0.09	0.18	--	2.43	0.08	1.17
0.500	Te	--	--	8.58	--	--	--	8.07	--
0.800	Th	--	[14]	13.72	[2]	--	--	12.92	--
0.005	Ti	--	4.01	0.09	0.46	--	[0.15]	0.08	[0.07]
0.250	Tl	--	--	4.29	--	--	--	4.04	--
2.000	U	--	--	34.31	--	--	--	32.30	--
0.015	V	--	--	0.26	--	--	--	0.24	--
0.500	W	--	--	8.58	--	--	--	8.07	--
0.010	Y	--	--	0.17	--	--	--	0.16	--
0.020	Zn	[0.89]	20.6	0.34	2.4	--	[0.45]	0.32	[0.22]
0.025	Zr	--	181	0.43	21	--	--	0.40	--

Note: 1) Overall error greater than 10-times detection limit is estimated to be within +/- 15%.

2) Values in brackets [] are within 10-times detection limit with errors likely to exceed 15%

3) "--" indicate measurement is below detection. Sample detection limit may be found by multiplying "det. limit" (far left column) by "multiplier" (top of each column).

